

Isobaric Vapor–Liquid Equilibria for Binary and Ternary Systems Composed of 2-Methoxy-2-methylpropane, Ethanol, 2-Methyl-2-propanol, and Octane at 101.3 kPa

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Isobaric vapor–liquid equilibria for two ternary systems, 2-methoxy-2-methylpropane (MTBE) + ethanol + 2-methyl-2-propanol and ethanol + 2-methyl-2-propanol + octane, and one binary system, ethanol + 2-methyl-2-propanol, have been measured at 101.3 kPa. The measurements were made in an equilibrium still with circulation of both the vapor and liquid phases. Both ternary systems and the binary system ethanol + 2-methyl-2-propanol do not form azeotropes. The three constituent binary systems of MTBE + ethanol, MTBE + 2-methyl-2-propanol, and 2-methyl-2-propanol + octane, which were measured in our previous work, are also not azeotropes. The other constituent system ethanol + octane, measured in our previous work, forms a minimum azeotrope. The experimental data for the binary systems were correlated with the nonrandom two-liquid (NRTL) equation. The NRTL equation yielded a good prediction of activity coefficients for the ternary systems from the parameters of the correlated binary systems.

Introduction

Ethers and alcohols used as gasoline additives have excellent antiknock qualities and are considered environmental protection substances. Gasoline including 2-methoxy-2-methylpropane (MTBE) has been used for a high-performance premium gasoline. In recent years, mixtures of ethers with alcohols have been considered for blending with gasoline. As a continuation of our studies^{1,2} on the vapor–liquid equilibrium (VLE) of MTBE + octane + alcohols systems, the isobaric VLE for the ternary systems MTBE + ethanol + 2-methyl-2-propanol and ethanol + 2-methyl-2-propanol + octane and the constituent binary system ethanol + 2-methyl-2-propanol have been measured at 101.3 kPa. The measurements were made in an equilibrium still³ with circulation of both the vapor and liquid phases. Data for the other four constituent binary systems of MTBE + ethanol,¹ MTBE + 2-methyl-2-propanol,² 2-methyl-2-propanol + octane,² and ethanol + octane⁴ were reported in our previous studies. For the ethanol + 2-methyl-2-propanol system, one set of isobaric VLE data at 101.3 kPa is reported by Suska et al.⁵ and one set of isothermal data at 313.15 K have been measured by Oracz.⁶ No isobaric or isothermal VLE data have been reported previously for the MTBE + ethanol + 2-methyl-2-propanol and ethanol + 2-methyl-2-propanol + octane systems.

Experimental Section

Materials. Ethanol, 2-methyl-2-propanol, and octane, supplied by the Wako Pure Chemical Co. Ltd., and MTBE, supplied by the Merck–Dr. Th. Schuchardt & Co., were special grade reagents. Ethanol was used after a small quantity of water was removed with 3A molecular sieves. Gas-chromatographic analysis on all three materials indicated that each had a purity of at least 99.9 mol %. The measured physical properties of the compounds are listed

Table 1. Normal Boiling Points, T_b , and Refractive Index, n_D , of the Components

material	T_b /K			n_D (298.15 K)	
	exptl	calc ^a	lit.	exptl	lit.
MTBE	328.14	328.36	328.11 ^b	1.366 41	1.3663 ^b
ethanol	351.44	351.45	351.443 ^c	1.359 37	1.35941 ^c
2-methyl-2-propanol	355.53	355.49	355.50 ^c	1.384 90	1.39389 ^c
octane	398.80	398.82	398.823 ^c	1.395 15	1.39565 ^c

^a Calculated value using the Antoine constants with Table 2.
^b Arce et al.¹¹ ^c Riddick et al.¹²

in Table 1 along with the literature data. Refractive index values were determined with a digital refractometer by using the critical angle of total reflection method (Kyoto Electric RA-510, Japan). Refractive index was measured with an accuracy of ± 0.00005 .

Procedure. An all Pyrex-glass equilibrium still with circulation of vapor and liquid phases, developed in a previous study,³ was used for the determination of VLE values. The overall charge of the apparatus was about 100 cm³ of solution.

The temperature was measured with a calibrated platinum resistance thermometer (Pt 100 Ω) with an accuracy of 0.03 K. A standard resistance thermometer (Chino Co. model R800-2, Japan), calibrated on the ITS-90 scale, was used for this calibration. The pressure in the apparatus was measured by means of a silicon resonant precision barometer (Tokyo Suzuki Seisakusho Co., model T60, Japan) with an accuracy of 0.015 kPa. Since the barometric pressure changed slightly, the experimental temperatures were corrected to 101.3 kPa.¹

Analysis. The equilibrium composition of the samples was determined by using a gas chromatograph (GL Sciences model GC-380, Japan) equipped with a flame ionization detector and an autosampler. The column packing was Gasukuropack 54 (supplied by the GL Sciences Inc.). The

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Table 2. Antoine Constants of the Components^a

material	A	B	C	ref
MTBE	6.120 19	1190.420	-39.040	<i>b</i>
ethanol	7.242 22	1595.811	-46.702	<i>c</i>
2-methyl-2-propanol	6.352 72	1105.198	-101.256	<i>c</i>
octane	6.043 94	1351.938	-64.030	<i>c</i>

^a $\log(P/\text{kPa}) = A - B/[(TK) + C]$. ^e Tsuji et al.¹³ ^f Boublik et al.¹⁴

Table 3. Isobaric Vapor–Liquid Equilibrium Data, Temperature, *T*, Liquid Phase, *x*₁, and Vapor Phase, *y*₁, Mole Fractions, and Activity Coefficient, γ_i , for the Ethanol (1) + 2-Methyl-2-propanol (2) System at 101.3 kPa

<i>TK</i>	<i>x</i> ₁	<i>y</i> ₁	γ_1	γ_2
355.53	0.0000	0.0000		
355.43	0.0343	0.0371	0.9257	0.9998
355.35	0.0721	0.0779	0.9273	0.9997
355.29	0.0978	0.1056	0.9293	0.9997
355.24	0.1175	0.1269	0.9314	0.9993
355.12	0.1727	0.1861	0.9333	0.9986
354.95	0.2402	0.2586	0.9390	0.9973
354.78	0.3020	0.3249	0.9443	0.9951
354.70	0.3341	0.3595	0.9477	0.9928
354.49	0.3996	0.4296	0.9546	0.9889
354.41	0.4236	0.4556	0.9576	0.9861
354.26	0.4650	0.4993	0.9616	0.9828
354.02	0.5284	0.5661	0.9686	0.9757
353.87	0.5636	0.6027	0.9724	0.9710
353.76	0.5904	0.6306	0.9755	0.9663
353.67	0.6110	0.6510	0.9766	0.9646
353.43	0.6618	0.7017	0.9808	0.9579
353.35	0.6776	0.7182	0.9835	0.9519
353.22	0.7033	0.7430	0.9853	0.9483
352.97	0.7524	0.7902	0.9892	0.9373
352.58	0.8224	0.8544	0.9936	0.9209
352.48	0.8408	0.8706	0.9943	0.9169
352.26	0.8780	0.9023	0.9952	0.9115
352.18	0.8919	0.9140	0.9957	0.9084
352.06	0.9121	0.9309	0.9965	0.9020
351.94	0.9303	0.9457	0.9969	0.8978
351.91	0.9347	0.9492	0.9971	0.8969
351.87	0.9417	0.9549	0.9973	0.8944
351.71	0.9659	0.9739	0.9977	0.8915
351.44	1.0000	1.0000		

relationship between peak area and composition was determined from analysis of samples of known composition. The accuracies of liquid, *x*_{*b*}, and vapor, *y*_{*b*}, mole fractions are estimated to be 0.002 mole fraction.

Experimental Results

The activity coefficients γ_i were calculated with the equation

$$Py_i = \gamma_i P_i^S x_i \quad (1)$$

In most cases it is preferable to calculate the activity coefficients by including fugacity coefficients and the Poynting factor correction. However, not all the required physical property data are available for MTBE to calculate these terms accurately. The activity coefficients were therefore calculated on the assumption of an ideal vapor phase. The vapor pressures of the pure components, P_i^S , were obtained using the Antoine equation constants, which are shown in Table 2.

Binary System. The binary VLE data for ethanol (1) + 2-methyl-2-propanol (2) are reported in Table 3 along with the activity coefficients calculated using eq 1. The values of $\ln \gamma_i$ are negative for the whole concentration range. The ethanol + 2-methyl-2-propanol system is nonazeotropic.

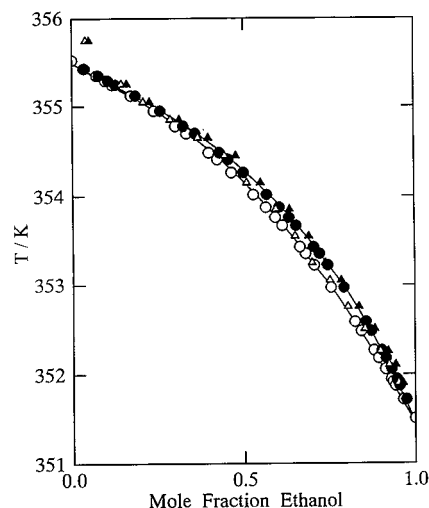


Figure 1. Temperature–composition diagram for ethanol (1) + 2-methyl-2-propanol (2) at 101.3 kPa. Present work: \circ , *x*₁; \bullet , *y*₁. Suska et al.⁵ at 101.3 kPa (1970): \triangle , *x*₁; \blacktriangle , *y*₁. —, NRTL equation with parameters from Table 6.

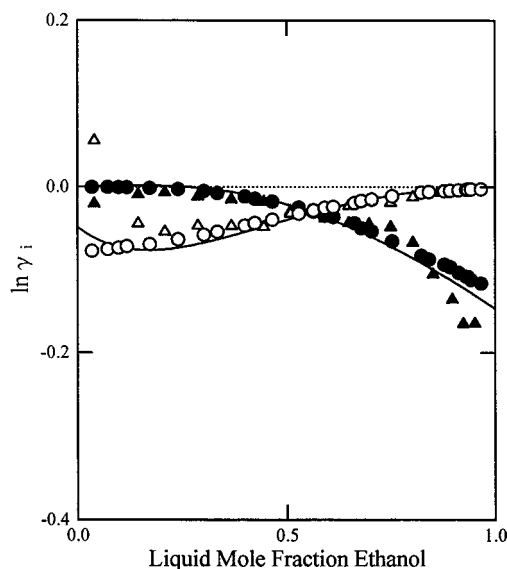


Figure 2. Activity coefficient–liquid composition diagram for ethanol (1) + 2-methyl-2-propanol (2) at 101.3 kPa. Present work: \circ , $\ln \gamma_1$; \bullet , $\ln \gamma_2$. Suska et al.⁵ at 101.3 kPa (1970): \triangle , $\ln \gamma_1$; \blacktriangle , $\ln \gamma_2$. —, NRTL equation with parameters from Table 6.

The experimental VLE for the ethanol (1) + 2-methyl-2-propanol (2) system is shown graphically in Figures 1 and 2.

The three constituent binary systems of MTBE + ethanol, MTBE + 2-methyl-2-propanol, and 2-methyl-2-propanol + octane, which were measured in our previous work, are nonazeotropes. As seen in our previous work, the other constituent system, ethanol + octane, forms a minimum boiling azeotrope.

The experimental data were tested for thermodynamic consistency using the point test of Fredenslund et al.⁷ and of Van Ness et al.⁸ The area test is not employed in this case because this system is almost ideal. The results indicate that the experimental data for the binary system of ethanol + 2-methyl-2-propanol are thermodynamically consistent.

Ternary System. The experimental VLE data for the ternary system MTBE (1) + ethanol (2) + 2-methyl-2-propanol (3) at 101.3 kPa are reported in Table 4. The tie lines and isotherms based on the experimental data for the

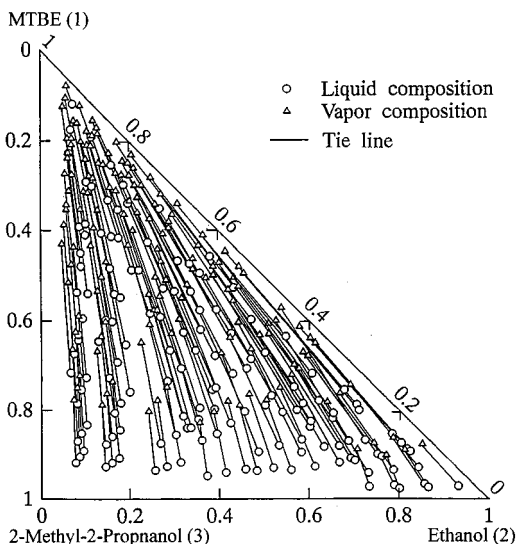


Figure 3. Tie lines for the ternary system MTBE (1) + ethanol (2) + 2-methyl-2-propanol (3) at 101.3 kPa: ○, liquid composition; △, vapor composition.

Table 6. Parameters of the NRTL Equation for the Binary Systems

system	$g_{ij} - g_{ii}$ J·mol ⁻¹	$g_{ij} - g_{jj}$ J·mol ⁻¹	α_{ij}
MTBE (1) + ethanol (2)	791.988	2501.984	0.47
ethanol (1) + 2-methyl-2-propanol (2)	3108.461	-2282.054	0.47
MTBE (1) + 2-methyl-2-propanol (2)	-793.364	2825.310	0.47
2-methyl-2-propanol (1) + octane (2)	2355.785	2188.091	0.47
ethanol (1) + octane (2)	5419.983	5029.721	0.47

5 and 6. Each of these systems forms a nonazeotropic mixture.

Correlation and Prediction

The activity coefficients were correlated with the non-random two-liquid (NRTL) equation (eq 9) using the α term as either a fitting parameter or a fixed value. In the case of the systems containing an alcohol with a hydrocarbon or an ether, it was acceptable to correlate using the fixed value of 0.47 as the α term. The parameters in the equation were obtained by using the Marquardt method.¹⁰ The sum of the squares of the relative deviations in the activity coefficients was minimized during optimization of the parameters.

The NRTL parameters, $g_{ij} - g_{ii}$, $g_{ij} - g_{jj}$, and α_{ij} for the five binary systems $i-j$ were determined on the basis of the experimental data. They are shown in Table 6. The calculated results using the NRTL equation are depicted by solid lines in Figures 1 and 2. The average absolute deviations and maximum deviations between the experimental and calculated vapor-phase compositions and tem-

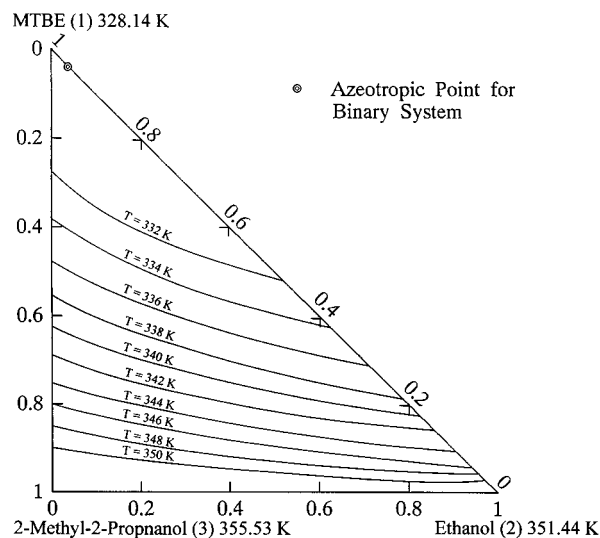


Figure 4. Isotherms for the ternary system MTBE (1) + ethanol (2) + 2-methyl-2-propanol (3) at 101.3 kPa.

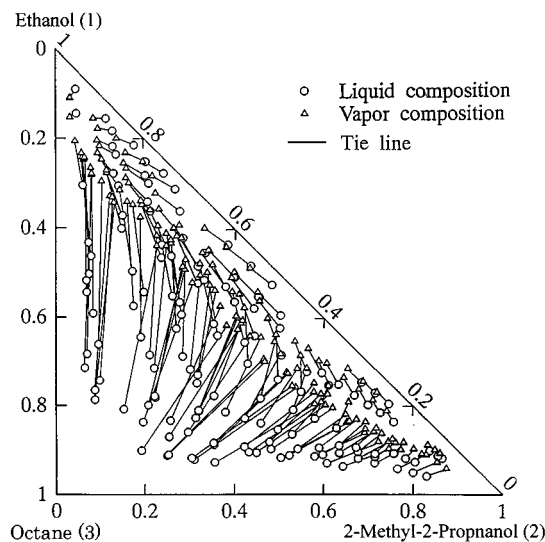


Figure 5. Tie lines for the ternary system ethanol (1) + 2-methyl-2-propanol (2) + octane (3) at 101.3 kPa: ○, liquid composition; △, vapor composition.

peratures for the constituent five binary systems are shown in Table 7.

The prediction of the ternary VLE was carried out with the NRTL binary parameters in Table 6. For the MTBE (1) + ethanol (2) + 2-methyl-2-propanol (3) system, the average absolute deviations were 0.007 mole fraction in y_1 , 0.004 mole fraction in y_2 , and 0.27 K in temperature. Average absolute deviations of 0.006 mole fraction in y_1 , 0.05 mole fraction in y_2 , and 0.18 K in temperature were

Table 7. Deviations between Calculated and Experimental Vapor Mole Fractions, Δy_b , and Temperatures, ΔT , of the NRTL Equation for the Binary Systems

system	deviation							
	average				maximum			
	Δy_1	$\Delta T/K$	$\Delta \gamma_1$	$\Delta \gamma_2$	Δy_1	$\Delta T/K$	$\Delta \gamma_1$	$\Delta \gamma_2$
MTBE (1) + ethanol (2) ^a	0.006	0.13	0.0130	0.0365	0.023	0.46	0.0483	0.0645
ethanol (1) + 2-methyl-2-propanol (2)	0.001	0.02	0.0044	0.0022	0.002	0.05	0.0184	0.0044
MTBE (1) + 2-methyl-2-propanol (2) ^b	0.003	0.12	0.0279	0.0289	0.007	0.46	0.1066	0.0971
2-methyl-2-propanol (1) + octane (2) ^b	0.006	0.12	0.0122	0.1118	0.014	0.35	0.0467	0.2845
ethanol (1) + octane (2) ^c	0.006	0.07	0.0244	0.0512	0.014	0.31	0.0640	0.0885

^a Reference 1. ^b Reference 2. ^c Reference 4.

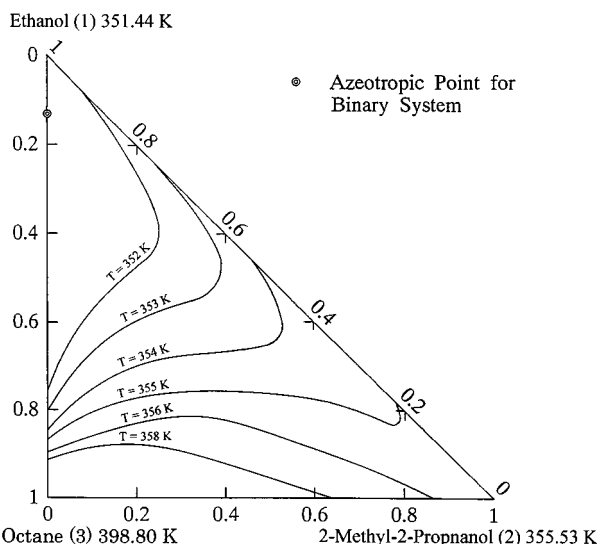


Figure 6. Isotherms for the ternary system ethanol (1) + 2-methyl-2-propanol (2) + octane (3) at 101.3 kPa.

determined for the ethanol (1) + 2-methyl-2-propanol (2) + octane (3) system.

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